

# GUJARAT TECHNOLOGICAL UNIVERSITY

BE-3 SEMESTER – OLD PAPER – S22 TO W25 – QUESTION BANK ANSWER

Subject Name & Code:

**FLUID FLOW OPERATIONS (3130502)**

**(Disclaimer:** The purpose of these AI-generated responses is just education and reference. Utilise them to grasp topics and structure, but always rewrite in your own words and double-check)

## Unit 4: Flow of Compressible Fluids

**Q1 – Define Mach number and explain its significance. (3 marks)**

**Appeared in:** S24 (Q4a, 03 marks), S23 (Q4a, 03 marks), S22 (Q3a OR, 03 marks) →

Highest: 3 marks

**Ans:**

**Definition:** Mach number (Ma) is the ratio of flow velocity (V) to the speed of sound (c) in the same medium at the same state.

$$Ma = V / c$$

**Significance:**

- **Ma < 0.3** → Incompressible flow (density changes <5%) – use Bernoulli's equation.
- **0.3 < Ma < 0.8** → Subsonic compressible flow – density variations matter.
- **Ma ≈ 1** → Transonic flow – shock waves begin.
- **Ma > 1** → Supersonic flow – expansion fans, oblique shocks.
- Determines flow regime for nozzle/diffuser design.

**Real-world application:**

- Aircraft design (subsonic vs supersonic).
- Rocket nozzle performance.
- Gas pipeline sizing (choking at Ma=1).

**Q2 – Explain isentropic flow of compressible fluid through nozzles. (7 marks)**

**Appeared in:** S23 (Q4b, 04 marks), S22 (Q3c OR, 07 marks), W25 (Q4c, 07 marks) →

Highest: 7 marks

**Ans:**

**Definition:** Isentropic flow is **adiabatic and reversible** (no friction, no heat transfer, no shocks). For a nozzle, it converts **pressure energy into kinetic energy** (velocity increases, pressure and temperature drop).

**Key equations for isentropic nozzle flow (ideal gas):**

1. **Continuity:**  $\dot{m} = \rho A V = \text{constant}$ .
2. **Energy (Steady flow):**  $h_1 + V_1^2/2 = h_2 + V_2^2/2 = h_0$  (stagnation enthalpy) → for ideal gas:  $C_p T_0 = C_p T + V^2/2$ .
3. **Isentropic relations:**  $P/\rho^k = \text{constant}$ ,  $T/P^{(k-1)/k} = \text{constant}$ .

**Velocity at any section:**

$$V = \sqrt{2 C_p (T_0 - T)} = \sqrt{2 \left( \frac{k}{k-1} \right) R T_0 \left( 1 - (P/P_0)^{(k-1)/k} \right)}$$

**Mass flow rate through nozzle:**

$$\dot{m} = P_0 A / \sqrt{T_0} \times \sqrt{\left[ \frac{k}{R} \right] \left( \frac{2}{k+1} \right)^{(k+1)/(k-1)}} \quad \text{(at throat when choked)}$$

**Nozzle types based on back pressure ( $P_{\text{back}}$ ):**

Condition	Flow at throat	Exit flow
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Condition	Flow at throat	Exit flow
$P_b > P_{critical}$	Subsonic ( $Ma < 1$ )	Subsonic
$P_b = P_{critical}$	Sonic ( $Ma = 1$ )	Subsonic or supersonic (depending on nozzle shape)
$P_b < P_{critical}$	Sonic ( $Ma = 1$ ) (choked)	Supersonic (convergent-divergent nozzle)

**[DG PROMPT]**

**Title:** Convergent-divergent nozzle – isentropic flow

**Description:** Draw a nozzle symmetric about horizontal axis. Left side: converging section (decreasing area) labelled “Convergent”. Middle: throat (minimum area) labelled “Throat ( $Ma=1$ )”. Right side: diverging section (increasing area) labelled “Divergent”. Arrows from left to right. Label inlet:  $P_0, T_0, V \approx 0$  (stagnation). Throat:  $Ma=1, P, T$ . Exit:  $P_{exit}, T_{exit}, V_{exit}$  (supersonic). Below, plot  $P/P_0$  vs distance along nozzle showing pressure drop.

**Real-world application:**

- Rocket engine nozzles (supersonic exhaust).
- Steam turbine nozzles.
- Supersonic wind tunnels.

**Numerical example:**

Air ( $k=1.4, R=287 \text{ J/kg}\cdot\text{K}$ ) flows isentropically through a nozzle. Stagnation conditions:  $P_0=500 \text{ kPa}, T_0=400 \text{ K}$ . Find velocity at a section where  $P=300 \text{ kPa}$ .

Solution:  $V = \sqrt{[2 \times (1.4/0.4) \times 287 \times 400 \times (1 - (300/500)^{0.4/1.4})]} = \sqrt{[2 \times 3.5 \times 287 \times 400 \times (1 - 0.6^{0.2857})]} = \sqrt{[803600 \times (1 - 0.876)]} = \sqrt{[803600 \times 0.124]} = \sqrt{99646} \approx 316 \text{ m/s}$ .

**Q3 – Derive expression for critical pressure ratio ( $r_{c}$ ) for isentropic flow. (4 marks)**

**Appeared in:** W25 (Q4b, 04 marks) → Highest: 4 marks

**Ans:**

**Definition:** Critical pressure ratio is the ratio of pressure at throat (where  $Ma=1$ ) to stagnation pressure:  $r_c = P^*/P_0$ .

**Derivation from isentropic relations:**

For isentropic flow:  $T_0/T = 1 + [(k-1)/2] Ma^2$ .

At  $Ma=1$  (throat):  $T_0/T^* = 1 + (k-1)/2 = (k+1)/2 \rightarrow T^* = T_0 \times 2/(k+1)$ .

From isentropic P-T relation:  $(P_0/P) = (T_0/T)^{k/(k-1)}$

Substitute  $T_0/T^* = (k+1)/2$ :

$$P_0/P^* = [(k+1)/2]^{k/(k-1)}$$

Therefore:

$$P^*/P_0 = [2/(k+1)]^{k/(k-1)}$$

**For common gases:**

- Air ( $k=1.4$ ) →  $P^*/P_0 = [2/2.4]^{1.4/0.4} = (0.8333)^{3.5} = 0.5283$ .
- Monatomic ( $k=1.67$ ) →  $P^*/P_0 \approx 0.487$ .
- Steam ( $k=1.3$ ) →  $P^*/P_0 \approx 0.546$ .

**Real-world application:**

- Nozzle design – choking occurs when back pressure  $\leq P_0 \times r_c$ .
- Orifice meters – critical flow condition for mass flow measurement.

**Example:** Air nozzle with  $P_0=500 \text{ kPa}$ . Critical pressure =  $500 \times 0.5283 = 264.15 \text{ kPa}$ . If back pressure  $< 264 \text{ kPa}$ , flow is choked.

**OQ1 – Derive expression for effect of cross-sectional area on velocity for isentropic flow through nozzle. (3 marks)**

**Appeared in:** W25 (Q4a, 03 marks) → Highest: 3 marks

**Ans:**

**Derivation from continuity and momentum (area-velocity relation):**

Start with continuity:  $\rho A V = \text{constant} \Rightarrow d\rho/\rho + dA/A + dV/V = 0 \dots(1)$

Euler's equation for isentropic flow:  $dP/\rho + V dV = 0 \dots(2)$

Isentropic relation:  $dP = c^2 d\rho$  where  $c = \text{speed of sound} = \sqrt{(kP/\rho)} = \sqrt{(kRT)}$ .

From (2):  $c^2 d\rho = -\rho V dV \Rightarrow d\rho/\rho = -(V/c^2) dV = -Ma^2 dV/V \dots(3)$

Substitute (3) into (1):  $-Ma^2 dV/V + dA/A + dV/V = 0$

$\Rightarrow (1 - Ma^2) (dV/V) + dA/A = 0$

**Final relation:**

$$dA/A = (Ma^2 - 1) dV/V$$

**Implications:**

- **Ma < 1 (subsonic):**  $(Ma^2 - 1)$  negative → dA and dV opposite signs.
  - Convergent nozzle ( $dA < 0$ ) →  $dV > 0$  (velocity increases).
  - Divergent diffuser ( $dA > 0$ ) →  $dV < 0$  (velocity decreases).
- **Ma > 1 (supersonic):**  $(Ma^2 - 1)$  positive → dA and dV same sign.
  - Convergent nozzle ( $dA < 0$ ) →  $dV < 0$  (velocity decreases – not used).
  - Divergent nozzle ( $dA > 0$ ) →  $dV > 0$  (velocity increases).

**Real-world application:**

- Explains why supersonic nozzles must be divergent.
- Design of C-D nozzles for rockets.

**OQ2 – Explain asterisk condition and stagnation condition. Derive stagnation temperature expression. (4 marks)**

**Appeared in:** W24 (Q5b, 04 marks), W22 (Q5b, 04 marks) → Highest: 4 marks

**Ans:**

**Stagnation condition (denoted by subscript 0):**

- State of fluid brought to **rest isentropically** (velocity reduced to zero).
- Stagnation temperature ( $T_0$ ), stagnation pressure ( $P_0$ ), stagnation density ( $\rho_0$ ).

*\*Asterisk condition (denoted by superscript):*

- State at which **Mach number = 1** (sonic condition).
- Usually occurs at nozzle throat.
- Denoted as  $T^*$ ,  $P^*$ ,  $\rho^*$ ,  $A^*$ .

**Derivation of stagnation temperature expression (from energy equation):**

Steady flow energy equation (adiabatic, no work):

$h_0 = h + V^2/2$ . For ideal gas:  $h = C_p T$ .

$$C_p T_0 = C_p T + V^2/2$$

$$\Rightarrow T_0 = T + V^2/(2C_p)$$

Since  $C_p = kR/(k-1)$  and  $V = Ma \cdot \sqrt{(kRT)}$ :

$$V^2/(2C_p) = Ma^2 \cdot kRT / [2 \cdot kR/(k-1)] = Ma^2 \cdot T \cdot (k-1)/2$$

Thus:

$$T_0/T = 1 + [(k-1)/2] Ma^2$$

**For asterisk condition (Ma=1):**  $T_0/T^* = 1 + (k-1)/2 = (k+1)/2$ .

**Real-world application:**

- Gas turbine engine – stagnation temperature measured by thermocouple with recovery factor.
- Nozzle design –  $T^*$  determines throat conditions.

**Numerical example:**

Air at  $Ma=0.8$ ,  $T=300$  K,  $k=1.4$ . Find  $T_0$ .

$$T_0 = 300 \times [1 + 0.4/2 \times 0.8^2] = 300 \times [1 + 0.2 \times 0.64] = 300 \times 1.128 = 338.4 \text{ K.}$$

### Q3 – Explain concept of isothermal friction flow with diagram. (4 marks)

Appeared in: W24 (Q3b, 04 marks), W22 (Q3b, 04 marks) → Highest: 4 marks

Ans:

**Definition:** Isothermal friction flow is **compressible flow in a constant-area duct** with **friction** (wall shear) but **constant temperature** (heat transfer maintains isothermal condition).

**Assumptions:**

- Steady, one-dimensional flow.
- Constant temperature ( $T = \text{constant}$ ).
- Friction present (non-isentropic).
- Ideal gas.

**Key characteristics:**

- Pressure decreases along duct due to friction.
- Velocity increases (since  $\dot{m} = \rho AV$ ,  $\rho$  decreases as  $P$  decreases, so  $V$  increases).
- Mach number increases along duct.
- **Choking** occurs when  $Ma$  reaches 1 (maximum length  $L_{\text{max}}$ ).

**Governing equations:**

- Continuity:  $\rho V = \text{constant}$ .
- Equation of state:  $P = \rho RT$  ( $R$  constant).
- Momentum with friction:  $dP + \rho V dV + (4f/D) (\frac{1}{2}\rho V^2) dx = 0$ .

**Fanno line** (for adiabatic friction flow) is replaced by isothermal line.

**[DG PROMPT]**

**Title:** Isothermal friction flow in constant-area duct

**Description:** Draw a horizontal constant-area pipe. Left end: inlet with  $P_1$ ,  $V_1$ ,  $Ma_1 (<1)$ . Right end: outlet with  $P_2 (<P_1)$ ,  $V_2 (>V_1)$ ,  $Ma_2 (>Ma_1)$ . Along the pipe, add small wavy lines at wall to represent friction. Plot below: Pressure ( $P$ ) decreasing along  $x$ , Velocity ( $V$ ) increasing along  $x$ , Mach number ( $Ma$ ) increasing towards 1. Label choking point where  $Ma=1$ .

**Real-world application:**

- Long gas pipelines (natural gas transmission) – approximately isothermal due to ground heat transfer.
- Pneumatic conveying systems.

### Q4 – Barometric equation with nomenclature. (3 marks)

Appeared in: S22 (Q4a, 03 marks) → Highest: 3 marks

Ans:

**Definition:** Barometric equation gives **pressure variation with altitude** in an isothermal atmosphere (constant temperature).

**Derivation (hydrostatic + ideal gas):**

Hydrostatic:  $dP/dz = -\rho g$ .

Ideal gas:  $\rho = P/(RT)$ .

Combine:  $dP/dz = -(P/(RT)) g \Rightarrow dP/P = -(g/RT) dz$ .

Integrate from  $z=0$  ( $P=P_0$ ) to  $z$  ( $P=P$ ):

$$\ln(P/P_0) = -(g/RT) z$$

**Barometric equation:**

$$P = P_0 \exp(-gz / RT)$$

**Nomenclature:**

- $P$  = pressure at altitude  $z$  (Pa)
- $P_0$  = pressure at reference ( $z=0$ , usually sea level) (Pa)
- $g$  = acceleration due to gravity ( $\approx 9.81 \text{ m/s}^2$ )
- $R$  = specific gas constant ( $\text{J/kg}\cdot\text{K}$ )
- $T$  = absolute temperature (K) – assumed constant
- $z$  = altitude (m)

**Real-world application:**

- Altitude correction for aircraft instruments.
- Weather forecasting (pressure at different heights).
- Calibration of barometers.

**Example:**

Sea level  $P_0 = 101325 \text{ Pa}$ ,  $T = 288 \text{ K}$ ,  $R$  for air =  $287 \text{ J/kg}\cdot\text{K}$ . Find  $P$  at  $z = 1000 \text{ m}$ .

$$P = 101325 \times \exp(-9.81 \times 1000 / (287 \times 288)) = 101325 \times \exp(-9810 / 82656) = 101325 \times \exp(-0.1187) = 101325 \times 0.888 = 89976 \text{ Pa}.$$

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